

# Superresolution imaging using superoscillatory diffractive neural networks

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**Abstract.** Optical superoscillation enables far-field superresolution imaging beyond diffraction limits. However, existing superoscillatory lenses for spatial superresolution imaging systems still confront critical performance limitations due to the lack of advanced design methods and limited design degree of freedom. Here, we propose an optical superoscillatory diffractive neural network (SODNN) that achieves spatial superresolution for imaging beyond the diffraction limit with superior optical performance. SODNN is constructed by utilizing diffractive layers for optical interconnections and imaging samples or biological sensors for nonlinearity. This modulates the incident optical field to create optical superoscillatory optical spot and generate the superresolved focal spots. By optimizing diffractive layers with 3D optical field constraints under an incident wavelength size of  $\lambda$ , we achieved a superoscillatory optical spot and needle with a full width at half-maximum of 0.407 $\lambda$  at the far-field distance over 400 $\lambda$  without sidelobes over the field of view and with a long depth of field over 10 $\lambda$ . Furthermore, the SODNN implements a multiwavelength and multifocus spot array that effectively avoids chromatic aberrations, achieving comprehensive performance improvement that surpasses the trade-off among performance indicators of conventional superoscillatory lens design methods. Our research work will inspire the development of intelligent optical instruments to facilitate the applications of imaging, sensing, perception, etc.

Keywords: superresolution imaging; photonic neural networks; optical superoscillation.

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# **1** Introduction

The Abbe–Rayleigh diffraction limit of traditional optical equipment has always been an obstacle to the study of microand nanoscale objects.<sup>1,2</sup> Near-field microscopic imaging techniques, such as contact photography<sup>3</sup> and scanning near-field imaging,<sup>4,5</sup> capture evanescent fields by placing a probe or light-sensitive material extremely close to the object to achieve nanoscale resolution, which is not possible for imaging inside biological samples or encapsulated micro- and nanostructures. Far-field microscopic imaging technology is not restricted by the above bottlenecks. Some typical far-field microscopic imaging techniques, such as single-molecule localization (SML) microscopy<sup>6,7</sup> or stimulated emission depletion (STED),<sup>8,9</sup> have demonstrated the possibility of nanoscale imaging without capturing evanescent fields. However, SML microscopy and STED typically require intense beams to excite, deplete, or bleach fluorophores in a sample that produces photobleaching and phototoxicity in living samples.

Optical superoscillations are rapid subwavelength spatial variations of light intensity and phase that occur in complex electromagnetic fields formed by the precise interference of coherent waves, which provide an advanced method for far-field superresolution imaging beyond the diffraction limit.<sup>10,11</sup> To generate optical superoscillation, complicated lens design methods<sup>12–14</sup> have been proposed. Additionally, Fresnel zone plate (FZP) optimization design methods, including optimizing

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algorithms<sup>15–18</sup> and optimization-free algorithms,<sup>19,20</sup> have also been developed. However, the existing superoscillatory focusing-based imaging designs require a trade-off among performance indicators and have limited performance as follows: (1) strong sidelobes resulting in a small field of view (FoV),<sup>12,15,20</sup> (2) short working distances,<sup>13,15,16,19</sup> (3) limited depth-of-focus (DoF),<sup>15,17,18,21</sup> and (4) chromatic aberration caused by wavelength-dependent phase retardation,<sup>13,14,19,22</sup> which dramatically limit their applications.

The performance limitations of the existing superoscillatory imaging methods are mainly due to the optimization with twodimensional (2D) optical field constraints. These constraints include limited modulation element numbers or only ring-structured phase modulation, which substantially limits the degree of freedom in design space for optimizing performance. For example, the conventional superoscillatory lens design methods, such as the pinhole array mask<sup>11</sup> or FZPs,<sup>17</sup> require the following steps. First, the prolate ellipsoid function or Strehl ratio is used as the optimization function of the model. Then, the phase distribution of the superoscillatory lens is optimized with the constraints of full width at half-maximum (FWHM) of the superoscillatory spot  $I_{(x_i,y_i)}$  at the 2D position of  $(x_i, y_i)$ , and the sidelobe intensity  $I_{\sum_{(x_j,y_j)}}$  at a combination of the 2D positions  $\sum_{(x_i,y_i)}$  in the local FoV expressed by the distance r between the superoscillatory spot and sidelobes. The above optimization method can only achieve the design of a pinhole array mask with a limited element number or a simple FZP with the ringstructured phase modulation of 0 or 1, while the optimization

process requires a very complex formula decomposition process. Here, we propose constructing the superoscillatory diffraction neural networks, i.e., superoscillatory diffractive neural networks (SODNNs), that generate optical superoscillation in 3D and achieve superresolution imaging beyond the diffraction limits, as shown in Fig. 1(a). SODNN is constructed by utilizing diffractive layers to implement optical interconnections and imaging samples or biological sensors to implement nonlinearity. The conventional superoscillatory lens design methods usually optimize the 2D superoscillatory spot with sidelobes around the focus spot, as shown in Fig. 1(b). SODNN modulates the incident optical field to create optical superoscillation effects in 3D space and generates the superresolved focusing spots or optical superoscillatory needle, as shown in Fig. 1(c). The diffraction limit of existing photonic neural network systems is due to training neural networks without exploring the superoscillatory effects. By constructing the large-scale SODNN that optimizes the optical coefficients of a stack of diffractive layers to modulate the optical field in 3D space, we can generate superoscillation at any local regions without sidelobes across the FoV and with long working distance, long DoF, and achromatic spots for highperformance superresolution imaging.

## 2 Methods

The forward model of SODNN is based on angular spectrum representation. The complex-valued coherent input optical field  $U_{\lambda_k}$  at the wavelength  $\lambda_k$  (k = 1, 2, ..., N) is transformed by SODNN before the detection. We consider the diffractive modulation layers of SODNN in this work with the complex transform function of  $M_{\lambda_k}(\Delta H, z_i)$  that modulates the incident optical field to the output optical field at the plane with a distance of  $z_i$ . Here,  $\Delta H$  represents the relative height map of the diffractive elements in SODNN to generate optical path

difference and modulate the phase  $\phi_{\lambda_k}$  of incident optical field, which can be formulated as  $\Delta H = \lambda_k \phi_{\lambda k} / 2\pi \Delta n_{\lambda_k}$  with  $\Delta n_{\lambda_k}$ being the wavelength-dependent material refractive index. Then, the output optical fields at the wavelength  $\lambda_k$  at the output plane with a distance of  $z_i$  can be formulated as  $U'_{\lambda_k}(z_i) =$  $M_{\lambda_k}(\Delta H, z_i)U_{\lambda_k}$ , and the detector measures the intensity distribution of output optical fields that can be formulated as a nonlinear function such as the square of the complex optical field:  $I_{\lambda_{k}}(z_{i}) = |U'_{\lambda_{k}}(z_{i})|^{2} = |M_{\lambda_{k}}(\Delta H, z_{i})U_{\lambda_{k}}|^{2}$ . We optimize the relative height of diffractive elements at different modulation layers with 3D optical field constraints across different wavelength channels. The optimization of large-scale diffractive elements reduces chromatic aberration caused by wavelength-dependent phase retardation, thereby enhancing the system's robustness to wavelength variations.<sup>23</sup> For the multiwavelength SODNN, the total intensity distribution of different wavelengths at the output plane can be formulated as the superposition of detected intensity distribution at each wavelength:  $I(z_i) = \sum_{\lambda_i} I_{\lambda_i}(z_i)$ .

The SODNN is optimized with the 3D optical field constraints, which optimizes the shape of the superoscillatory focusing spot within a certain distance range  $z_i \in [f - \Delta f, f + \Delta f]$ before and after the focal plane with a focal length of f. The ideal superoscillatory focusing spot  $I_{(x_i,y_i,z_i)}$  at a position in the 3D space with coordinates  $(x_i, y_i, z_i)$  at the output plane with a distance of  $z_i$  would have a maximized energy focused spot  $I_{(x_i,y_i,z_i)}$  and minimized light intensity sidelobes  $I_{\sum_j (x_j,y_j,z_i)}$  at a combination of position coordinates  $\sum_{j} (x_j, y_j, z_i)$ . Taking the ideal output light intensity as the optimization direction with the entire 3D optical field constraints, the SODNN performs the function of a neuromorphic photonic processor that utilizes weighted optical diffractive interconnections of massively diffractive neurons to achieve the desired optical superoscillatory function. In addition, we further design the constraint to maximize the energy transmission efficiency of superoscillatory regions by minimizing the optical energy outside the superoscillatory regions. Therefore, the 3D optical field constraint optimization of SODNN can be formulated as

$$\min_{\Delta H} \left( \sum_{z_i \in [f - \Delta f, f + \Delta f]} \left( \left( \left( I_{(x_i, y_i, z_i)} + I_{\sum_j (x_j, y_j, z_i)} \right) - I_{\text{target}} \right)^2 + \text{MSE}(I_{(x, y, z) \notin (x_i, y_i, z_i)}) \right), \quad (1)$$

where  $I_{(x_i,y_i,z_i)}$  is the intensity of the superoscillatory focusing spot at the 3D position of  $(x_i, y_i, z_i)$ ;  $I_{\sum_j(x_j, y_j, z_i)}$  is the intensity of the sidelobes at the 3D positions of  $\sum_j (x_j, y_j, z_i)$ ;  $I_{\text{target}}$  is the ground-truth label that represents the ideal superoscillatory output;  $\text{MSE}(I_{(x,y,z)\neq(x_i,y_i,z_i)})$  represents the total energy of optical intensity outside the superoscillatory regions with the mean square error (MSE) function;  $z_i \in [f - \Delta f, f + \Delta f]$  is the range of the 3D optical field constraint optimization space before and after the focal plane with a focal length of f; and  $\Delta H$  is the relative height map of the diffractive elements.

For the design of SODNN in this work, we use the stochastic gradient descent approach to optimize the network coefficients on a desktop computer (Linux) with an Intel Xeon Gold 6226R CPU at 2.90 GHz with 16 cores, and an NVIDIA GTX-3090Ti GPU with 24 GB graphics card memory. The residual error of network outputs with respect to ground-truth labels and the total

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2D Focus Spot with Conventional Methods

3D Optical Field Constraints with SODNN

Fig. 1 Training SODNN to optimize the diffractive elements with 3D optical field constraints. (a) Utilizing diffractive modulation layers and free-space propagation to implement the weighted optical interconnections, and imaging samples or biological sensors to implement nonlinearity. SODNN can modulate the multiwavelength incident optical field to create optical superoscillation effects in 3D superoscillatory regions. (b) The conventional methods optimize a 2D focus spot at a specific focusing distance to achieve optical superoscillation with a large sidelobe. (c) The enlarged 3D superoscillatory regions show that SODNN optimizes the 3D optical field in a certain distance range to achieve superoscillation without the sidelobe.

optical energy outside the superoscillatory regions are calculated according to Eq. (1), which are used to perform the error backpropagation to optimize the SODNN and the relative height map  $\Delta H$  of the diffractive modulation elements in SODNN.

# 3 Results

## 3.1 Numerical Evaluations

We first validate the effectiveness of the 3D optical field constraint optimization of SODNN in achieving superoscillatory spots without sidelobes to realize a large FoV at the designed long focal length f, as shown in Figs. 2(a) and 2(b). Each optical diffractive element size was set to  $\lambda/2 \times \lambda/2$ , where  $\lambda$  is the wavelength of input coherent light, which is 632.8 nm. We designed a one-layer SODNN with a modulation element number of  $2500 \times 2500$ , corresponding to a network layer size of  $0.79 \text{ mm} \times 0.79 \text{ mm}$ . The selection of the above parameters was determined according to the performance analysis of SODNN, as discussed in Sec. 4.2. The proposed system forms a superoscillatory focused spot with almost no sidelobes at a long focal length  $f = 250 \ \mu m (\sim 400 \lambda)$ , with an FWHM of

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**Fig. 2** Optical superoscillatory spots and optical needle design of SODNN. The FWHM (a) and the output (b) of superoscillatory spots at the designed focal length and distributions offsetting the designed focal length with the collimated input optical field. (c) The optical superoscillatory needle within a DoF of 6  $\mu$ m with uniform light intensity and consistent FWHM. (d) The 3D distributions of the output optical superoscillatory needle. (e) The output of the slices of the optical superoscillatory needle.

258 nm [ $\sim$ 0.407 $\lambda$ ; this is shown in the middle of Fig. 2(a) and the lower left of Fig. 2(b)]. Recent achievements of the superoscillatory lenses compared with SODNN are shown in Sec. 4.1, which demonstrates the extraordinary performance of SODNN.

It can be found that optimizing the SODNN only at a designed focal length f [that is  $\Delta f = 0$  in Eq. (1)], SODNN can maintain the morphology of the superoscillatory focus spot and avoid the appearance of sidelobes at the designed position; once it exceeds this distance, the sidelobes will appear immediately accompanied by smaller FWHM and weaker superoscillatory focusing spot intensity. For example, at four different focal lengths  $f - 2\Delta f$ ,  $f - \Delta f$ ,  $f + \Delta f$ , and  $f + 2\Delta f$  where  $\Delta f = 0.25 \ \mu$ m, we found that the sidelobes appeared and the FWHM was reduced to 206 nm (~0.325 $\lambda$ ), 246 nm (~0.388 $\lambda$ ), 246 nm (~0.388 $\lambda$ ), and 206 nm (~0.325 $\lambda$ ), respectively, as shown in Figs. 2(a) and 2(b). For the out-of-focal planes, the intensity of the sidelobes increases exponentially with respect to the central spot as the central spot size decreases, demonstrating the high quality of optical sectioning of the SODNN for imaging.

In order to maintain the profiles of superoscillatory light spots within a long DoF range, that is, to form a superoscillatory light needle, we optimize the shape of the superoscillatory

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**Fig. 3** Multiwavelength and multifocus SODNNs. (a) The superoscillatory spots under red, green, and blue light channels with the FWHM of 259, 221, and 199 nm, respectively. (b) The 3 × 5 superoscillatory spot arrays under red, green, and blue light channels with the FWHM of 267, 222, and 199 nm, respectively. (c) The superoscillatory spots of the T-H-U pattern with the FWHM of 274 nm and the superoscillatory spots of the heart-shaped pattern with the FWHM of 262 nm.

focusing spot within a certain distance range  $[f - 6\Delta f, f + 6\Delta f]$ before and after the focal length f, as shown in Figs. 2(c)-2(e). Each optical diffractive element size was set to  $\lambda/2 \times \lambda/2$ , where  $\lambda = 632.8$  nm. We evaluate the performance of onelayer SODNN by setting the modulation element number to  $1500 \times 1500$ , corresponding to the network layer size of 0.47 mm  $\times$  0.47 mm. We set the range of the 3D optical field constraint optimization space  $z_i \in [f - 6\Delta f, f + 6\Delta f]$ , where  $f = 100 \ \mu \text{m}$  and  $\Delta f = 0.5 \ \mu \text{m}$ . We found that an optical superoscillatory needle was formed within a long DoF of 6  $\mu$ m [~10 $\lambda$ , see Fig. 2(d)]. The optical superoscillatory needle was further tested by selecting seven positions in the range  $[f - 6\Delta f, f + 6\Delta f]$  with  $2\Delta f$  as the sampling interval [see the slices of the optical superoscillatory needle in Fig. 2(e) and the FWHM in Fig. 2(c)]. It can be found the optical superoscillatory needle has uniform light intensity and consistent FWHM (250  $\pm$  3 nm) in the designed DoF.

Based on our earlier studies,<sup>23,24</sup> we further demonstrate the multiwavelength SODNN to solve the chromatic aberration problems caused by wavelength-dependent phase retardation,

as shown in Figs. 3(a) and 3(b). In this design, three different parallel wavelength channels [i.e., blue, green, and red light with the wavelengths of 473 nm ( $\lambda_1$ ), 532 nm ( $\lambda_2$ ), and 632.8 nm ( $\lambda_3$ ), respectively] are used to generate multiwavelength superoscillatory light spots focused at the same focal length. Each optical diffractive element size was set to  $\lambda_3/2 \times \lambda_3/2$ . We also designed a one-layer SODNN by setting the modulation element number to  $2500 \times 2500$ , corresponding to the network layer size of 0.79 mm  $\times$  0.79 mm. The proposed system forms multiwavelength superoscillatory focused spots with almost no sidelobes at a long focal length  $f = 250 \ \mu m (\sim 400 \lambda_3)$ , with the FWHM of 259, 221, and 199 nm, respectively, produced by red light, green light, and blue light, shown in Fig. 3(a), respectively. Using the integrated multifocus and multiwavelength design approach proposed above, we further design a multiwavelength multifocus SODNN, shown in Fig. 3(b), which can realize  $3 \times 5$  superoscillatory focusing spot arrays under red, green, and blue light channels. The  $3 \times 5$  superoscillatory focusing spot arrays were produced by red light, green light, and blue light with the FWHM of 267,

222, and 199 nm, respectively. The comparisons of the proposed SODNN with respect to the state-of-the-art achievements of superoscillatory designs are also discussed in Sec. 4.1. Some complex multifocus superoscillatory spots, such as heart-shaped pattern and T-H-U pattern (the abbreviation of Tsinghua University), are shown in Fig. 3(c) to demonstrate the superiority of SODNN in terms of design flexibility and versatility. For the above two multifocus arrays, we obtained the FWHM of 274 and 262 nm, respectively, beyond the diffraction limit  $(0.61\lambda/NA = 456 \text{ nm})$ .

#### 3.2 Experimental Evaluations

We built the experimental setup to measure the SODNN's superoscillatory focusing spot profiles, as shown in Fig. 4(a). A He-Ne laser (25-STP-912-230, Melles Griot) with a wavelength of 632.8 nm and a power of 5 mW was collimated by lens 1 and lens 2, and a pinhole was used as a filter. The collimated He-Ne laser beam was used to illuminate the SODNN placed on the multi-axis translation stage (NPXYZ100SGV6, Newport), which was processed by two-photon printing technology (Moji Nano Technology, China). Considering the error accumulation and processing costs of large-scale devices in actual processing, we designed two kinds of small-scale one-layer SODNNs with the modulation element number of  $200 \times 200$  corresponding to each optical diffractive element size of 500 nm × 500 nm and 1-bit step height of 0 and 500 nm to verify the correctness of SODNN. Figure 4(d) left and middle are, respectively, designed to achieve single-focus focusing and a  $2 \times 2$  multifocus array focusing of superoscillatory spots, while Fig. 4(d) right is the enlarged part of the processed  $2 \times 2$  multifocus SODNN after characterization by electron microscopy (EM). An Olympus objective ( $100 \times$  magnification, NA = 0.9) was used to image the light focused by the designed SODNNs. A tube lens with focal length f = 180 mm was used to form an image on a CMOS camera (01-MOMENT, Photometrics).

Figure 4(e) left and Fig. 4(f) left are the numerical analysis results of a single-focus superoscillatory focusing spot and  $2 \times 2$ multifocus superoscillatory focusing spot array with a focal length  $f = 20 \ \mu m$ , at its design wavelength  $\lambda = 632.8 \ nm$ . The spot morphology is highly consistent with the experimental measurement results shown in Fig. 4(e) middle and Fig. 4(f) middle. For the single-focus superoscillatory focusing spot and the  $2 \times 2$  multifocus superoscillatory focusing spot array, the FWHMs obtained by numerical analysis results are 307 nm [see Fig. 4(e) right] and 340 nm [see Fig. 4(f) right], respectively. However, due to the systematic errors during the optical processing, the experimentally measured FWHMs were 383 nm [see Fig. 4(e) right] and 392 nm [see Fig. 4(f) right], respectively. By utilizing an in situ training algorithm, e.g., adaptive training methods,<sup>25,26</sup> with the programmable diffractive layers, the system can adapt to a wide range of tuning errors, preserving performance during deployment. These strategies present a viable approach to enhance the robustness of SODNNs. Although there was a slight gap with the numerical results, the experimental results still exceeded the diffraction limit  $(0.61\lambda/NA = 415 \text{ nm}).$ 

For imaging, we used a scanning mode with SODNN, where the signal used to reconstruct the image is taken from the central part of the CMOS camera. This imaging strategy is also commonly used in confocal microscopy.<sup>27,28</sup> The experimental equipment is shown in Fig. 4(a), where the commercial resolution testing chart [TC-RT01, Technology Manufacture, Germany; see Fig. 4(b)] is used as the target for measurement. The resolution testing chart's pattern structure is achieved by processing metallic chromium (Cr) on a glass substrate ( $S_iO_2$ ) with the smallest line width of 0.152  $\mu$ m. The 500-line pair pattern that cannot be clearly imaged by a commercial Olympus objective [see Fig. 4(b)] can be clearly imaged through SODNN [see Fig. 4(c)], demonstrating that SODNN has a performance comparable to the commercial microscopy imaging system. A more compact solution is to integrate SODNN with optical fiber to form an endoscope, as described in Sec. 4.4.

## 4 Discussion

#### 4.1 Comparisons with State-of-the-Art Methods

Table 1 compares several typical performance indices of superoscillatory design with the proposed SODNN in this work. SODNN can achieve a long working distance with hundreds of micrometers, while the other works can only achieve a short working distance with only tens of micrometers. In terms of working distance, SODNN has achieved an improvement by an order of magnitude. SODNN can also achieve a DoF greater than 6  $\mu$ m, and the ratio of FWHM to Rayleigh diffraction limit is less than 60%, which indicates its exceptional imaging capabilities and overall performance.

#### 4.2 Performance Analysis of SODNN

We evaluate and compare the network performance under different modulation element numbers, i.e.,  $K \times K$ , with K = 100, 200, 300, 500, 1000, and 2500 [Fig. 5(a)] when the number of layers is fixed at 1, and the diffractive element size is  $\lambda/2 \times \lambda/2$ . We also evaluate the network performance under different layer numbers when the modulation element numbers are fixed at  $200 \times 200$  [Fig. 5(b)] and  $300 \times 300$  [Fig. 5(c)] and the diffractive element size is  $\lambda/2 \times \lambda/2$ . We also analyze the effects of changes in neuron size, i.e., the diffractive element size was set to  $\lambda/2 \times \lambda/2$ ,  $\lambda \times \lambda$ ,  $2\lambda \times 2\lambda$ , and  $4\lambda \times 4\lambda$  when the number of layers is fixed at 1 and modulation element number is  $300 \times 300$  [see Fig. 5(d)]. We found that as the number of layers increases and the number of neurons in each layer increases, the FWHM of the superoscillatory spot without sidelobes will gradually become smaller and stabilize at ~0.407 $\lambda$  [Figs. 5(a) and 5(c)]. It seems that the modulation element numbers have a greater impact than the layer numbers on the FWHM by comparing Figs. 5(b) and 5(c). When the modulation element numbers are small, no matter how the layer numbers increased, the FWHM of the superoscillatory spot without sidelobes cannot be stabilized at ~0.407 $\lambda$ . On the contrary, as the diffractive element size increases, the FWHM of the superoscillatory spot without sidelobes will gradually increase. The above results can guide system design, such that under specific system parameters, e.g., a one-layer SODNN with enough modulation element numbers, optimal performance comparable to a multilayer SODNN can be achieved, which thereby greatly reduces hardware complexity, system errors, and experimental difficulty and enhances robustness during system installation and adjustment.

## 4.3 Reconfigurable SODNN for Superoscillatory Spot Scanning

SODNN can modulate the incident optical field to create optical super oscillatory effects in any 3D space and generate



**Fig. 4** Characterization of SODNN. (a) Schematic of the experimental setup. (b), (c) Imaging results of the resolution testing chart by commercial Olympus objective and SODNN. (d) The diffractive modulation layer of single-layer SODNNs for a single-focus (left) and  $2 \times 2$  multifocus (middle) with the layer profile characterized by scanning electron microscope, i.e., SEM (right). (e) The numerical analysis results (left) and experimental results (middle) of the single-focus SODNN. (f) The numerical analysis results (left) and experimental results (middle) of the  $2 \times 2$  multifocus SODNN.

Method	Wavelength (nm)	Focal length (µm)	DoF (µm)	FWHM (λ)	Ratio of FWHM/Rayleigh diffraction limit ( $0.61\lambda/NA$ )	Ambient medium	Refs.
Monochromatic superoscillatory design	640	10	_	0.289	64%	Oil	12
	810	10	—	0.45	85%	Air	20
	632.8	38	_	0.45	71%	Air	21
Achromatic superoscillatory design	405	—	—	0.457	67%	—	—
	532	10	_	0.445	65%	Air	17
	633	—	_	0.54	79%	_	_
Optical superoscillatory needle design	532	6	~5	0.34	81%	Oil	18
	405	55	~4.8	0.407	~65%	Air	22
Monochromatic superoscillatory design by SODNN	632.8	250	—	0.407	57%	Air	This work
Achromatic superoscillatory design by SODNN	473	—	_	0.420	59%	_	_
	532	250	_	0.415	58%	Air	This work
	632.8	—	_	0.409	57%	_	_
Optical superoscillatory needle design by SODNN	632.8	100	6	0.395	60%	Air	This work

 Table 1
 Comparisons of SODNNs with state-of-the-art superoscillatory methods.



Fig. 5 Performance analysis of SODNN. The FWHM of the output spot with respect to the modulation element number (a), the layer number (b), (c), and the modulation element size (d).



**Fig. 6** Reconfigurable SODNN for superoscillatory imaging. The superoscillatory spot can raster scan over the field for imaging by dynamically programming the modulation coefficients of diffractive elements.

superresolved focusing spots. By training a series of SODNNs and loading them into a reconfigurable device such as a spatial light modulator (SLM), we can achieve dynamic scanning of superoscillatory spots. We designed a series of SODNNs by setting the modulation element number to  $2500 \times 2500$  with the element size  $\lambda/2 \times \lambda/2$  and  $\lambda = 632.8$  nm, which corresponds to the network layer size of 0.79 mm × 0.79 mm with the focal

length  $f = 250 \ \mu\text{m}$ . The FWHM remains at 258 nm (~0.407 $\lambda$ ) and does not change with the position of the superoscillatory spots. Figure 6 shows that SODNN can focus the superoscillatory spots at even the four most edge locations of the detection plane, which proves that SODNN can realize scanning at any position on the detection plane. Considering a high-speed SLM that works at 1000 frames per second and takes the



**Fig. 7** Integrating SODNN with optical fiber. (a) Schematic diagram of the endoscope designed by integrating SODNN and optical fiber. (b) The imaging function is realized by utilizing the intensity of reflected light produced by different transmittance structures, such as the metal structure producing a strong reflection (c) and the glass forming a weak reflection on the hypothetical observation plane (d).

FWHM as the scanning interval, the SODNN can achieve a scanning range of 66.56  $\mu$ m<sup>2</sup>/s.

## 4.4 Integrating SODNN with Optical Fiber

A more compact solution is to integrate SODNN with optical fiber to form an endoscope, as shown in Fig. 7(a), and collect the reflection signal of the superoscillatory focusing spot from the measured target to complete the imaging process. By using Lumerical FDTD to arrange a hypothetical observation plane at the input end of SODNN to capture the topography of the reflected light field, we found the metal structure produces strong reflection [see Fig. 7(c)] with a normalized light intensity of 1; the glass forms a weak reflection with the normalized light intensity ~0 [see Fig. 7(d)]. Using the binary change of light intensity, we can also reconstruct the 500-line pair pattern of the measured resolution testing chart [see Fig. 7(b)].

## 5 Conclusion

We proposed SODNNs that demonstrate unparalleled advantages over other techniques for the realization of superoscillatory spots and imaging beyond the diffraction limit. SODNNs make it possible to flexibly design large FoV without sidelobes, long working distances, long DoF, and achromatic optical superoscillatory functions. SODNNs can work at any wavelength, from microwaves to ultraviolet waves,<sup>29</sup> which makes it possible to obtain superoscillatory spots with a smaller FWHM and further improve the resolution of SODNN imaging. We believe that this is a new cross-innovation in the fields of photonic neural networks, superresolution microscopy, and metasurfaces that will attract the attention of more scientists engaged in the development of intelligent optical instruments.<sup>30–35</sup>

## Disclosures

The authors declare no competing interests.

## Code and Data Availability

All relevant code is available from the corresponding author upon reasonable request.

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